

Millington Bridge Pier Replacement



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Satyam Mandloi, E.I.
2022



Project Location – Kendall/LaSalle County



Summary

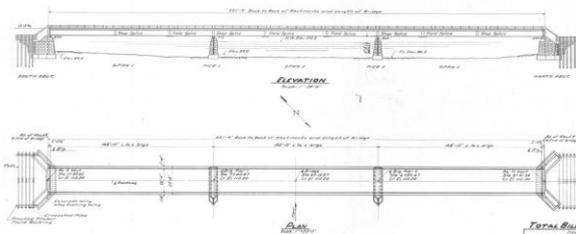
- Critical Scouring of soil beneath the pier resulting in settlement of bridge support as determined from routine bridge inspections by WHA.
- Temporary steel frames were used to support the bridge deck and girders in place.
- The existing pier was replaced by the reinforced-concrete strut-tie piers spanning between two battered-steel-pile-supported foundations.
- Pier replacement was completed successfully, and the bridge is now under operation.

Existing Bridge Info

- The existing bridge is a three-span reinforced concrete deck bridge supported by riveted plate girders. The total length back-to-back of abutments is 451'-9". The spans are: 148'-10", 150'-0" and 148'-10". The out-to-out width of the structure is 25'-8". The substructure consists of closed masonry abutments and solid masonry piers supported on spread footings. The structure was built as Millington Bridge in 1958, rehabilitated in 2000, and painted in 2015.

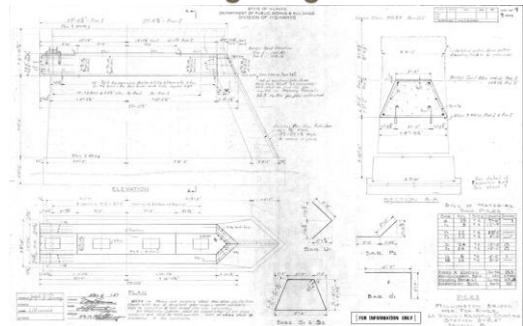


Existing Bridge Info



General Plan & Elevation (1958 Plans)

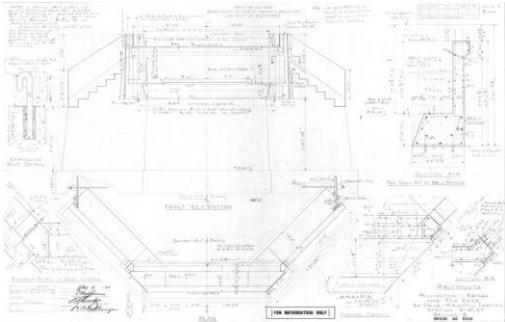
Existing Bridge Info



Piers (1958 Plans)

Note: We don't know exactly when the pier was built.

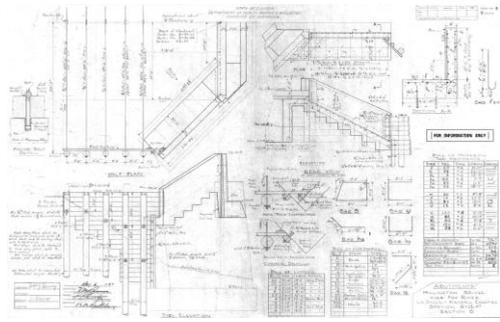
Existing Bridge Info



Abutments (1958 Plans)

7

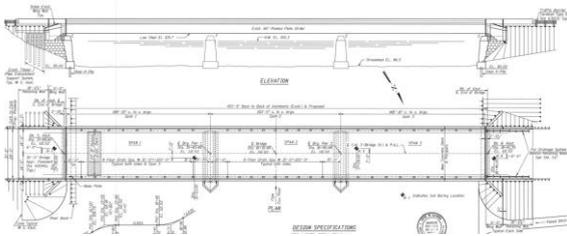
Existing Bridge Info



Abutments (1958 Plans)

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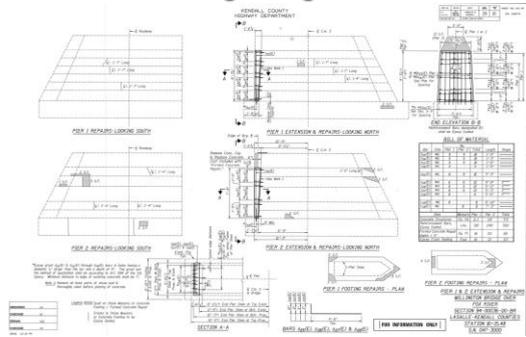
Existing Bridge Info



General Plan & Elevation (2000 Plans)

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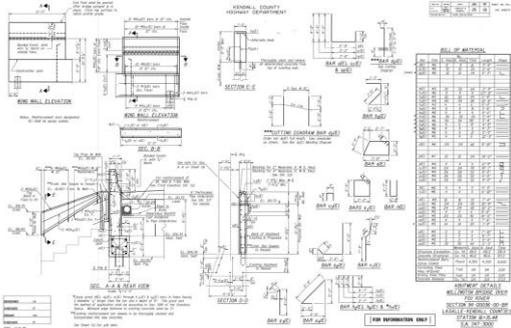
Existing Bridge Info



Piers (2000 Plans)

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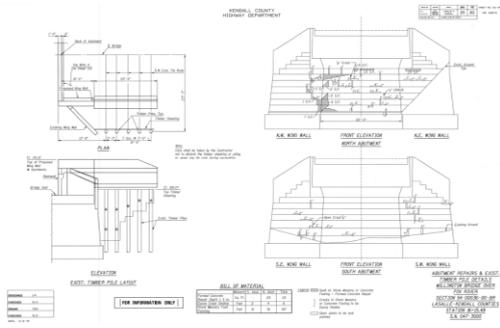
Existing Bridge Info



Abutments (2000 Plans)

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Existing Bridge Info



Abutments (2000 Plans)

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Existing Bridge Info



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Existing Bridge Info



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Existing Bridge Info



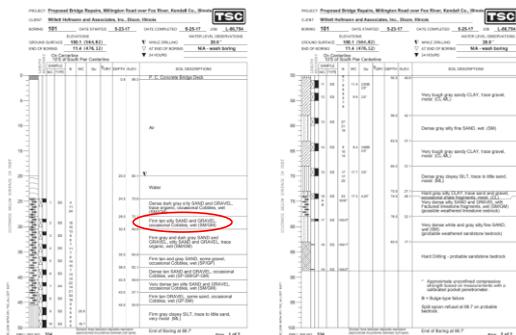
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Underwater Inspection

- WHA performs routine bridge inspections for LaSalle and Kendall counties.
- WHA found scour underneath the north pier and deemed further investigation was required to figure what the pier was actually resting on.
- WHA contracted Collins Engineering Inc. to perform underwater inspection of the scoured pier with the help of divers.
- WHA surveyed the bridge and ascertained that the bridge deck over north pier settled an inch.
- The problem was that the piers 1 and 2 consist of a solid stone masonry pier founded on concrete spread footing resting on firm tan silty sand and gravel.

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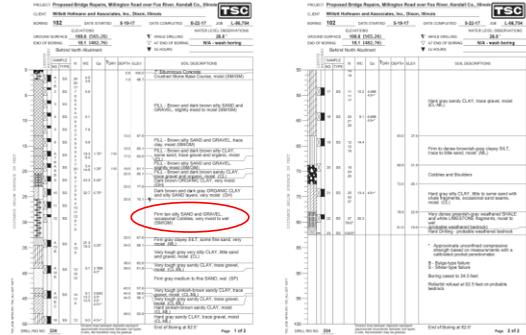
Underwater Inspection



Pier 1 Borings (South Pier)

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Underwater Inspection

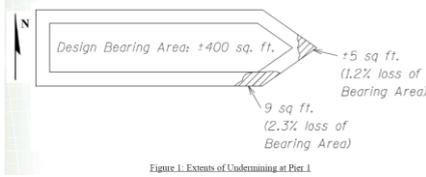


Pier 2 Borings (North Pier)

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Underwater Inspection

- Pier 1 (South Pier) was in poor condition at the time of inspection. Two areas of footing undermining were observed at the upstream nose and the southeast corner of the pier.



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Underwater Inspection



Photograph 3: Overall View of Pier 1 (South Pier), Looking Northeast.

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Underwater Inspection

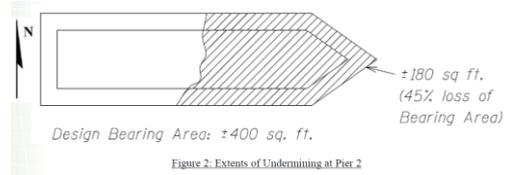


Photograph 4: Overall View of Pier 1 (South Pier), Looking Southwest.

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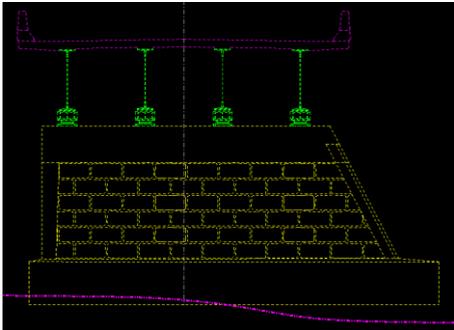
Underwater Inspection

- Pier 2 (North Pier) was in critical condition at the time of inspection. Channel bottom scour and footing undermining was observed at the upstream half of the pier.



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Underwater Inspection



Scour at Pier 2 (North Pier)

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Underwater Inspection



Photograph 5: Overall View of Pier 2 (North Pier), Looking Northeast.

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Pier Retrofit Analysis Evaluation or Replacement

- WHA hired Benesch as a pier reviewer to aid in evaluating pier retrofit alternatives to present to Kendall/LaSalle County.
- Seven (7) pier retrofit alternatives were deemed feasible.
- The best retrofit alternative was compared against complete replacement.

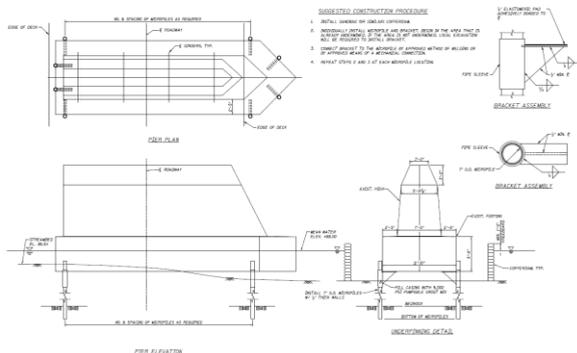
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Alternative 1, Micropile and Bracket Underpinning

- Alternative 1 proposes the use of micropiles and a bracket assembly to underpin the existing footing.
- This alternative would require a shallow cofferdam to provide access for the installation of the underpinning brackets.
- This alternative directly transfers the load from the existing footing to the bracket to the micropile.
- The connection between the bracket and the micropile will be the weak point of the system. This creates an inefficient use of the micropiles increasing the amount of required micropiles.
- A potential drawback to this system is the geometry of the existing footing could create significant challenges to obtaining an effective transfer of force to the bracket.

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Alternative 1, Micropile and Bracket Underpinning



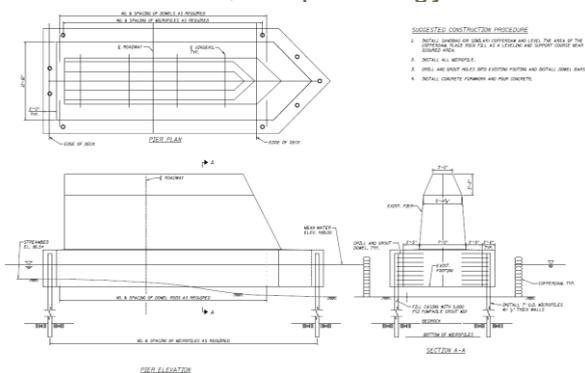
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Alternative 2, Micropile Footing Jacket

- To mitigate the concerns about engaging the footing via a bracket, Alternative 2 utilizes micropiles driven around the outside of the existing footing.
- After the micropiles are installed, dowel bars will be installed into the existing footing and concrete will be placed to create a force transfer from the existing footing, through the bars and into the micropiles.
- This alternate has two significant drawbacks:
 - The condition of the existing footing may be too deteriorated to provide adequate bonding and load transfer to the new footing jacket.
 - The footing jacket would also increase the total width by 2'-0" on every side of the existing footing, and therefore, the hydraulic opening will decrease.

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Alternative 2, Micropile Footing Jacket



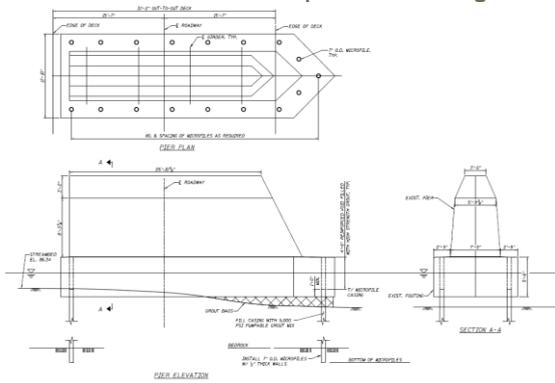
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Alternative 3, Micropile Thru Footing

- With the understanding that hydraulic impacts need to be avoided, Alternative 3 involves drilling micropiles through the existing footing.
- This alternative transfers the load directly from the footing to the micropiles via the bond between the grout and the existing footing.
- While this solution maintains a simpler load path, it still relies on the existing footing to transfer load.
- This option is also difficult to construct as the micropile equipment would have to work on the uneven surface of the existing footing and the drilled hole would have to be constructed so as to not compromise the integrity of the footing.

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Alternative 3, Micropile Thru Footing



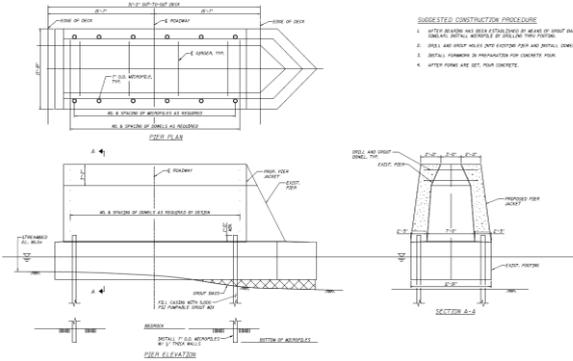
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Alternative 4, Micropile with Pier Jacket

- Alternative 4 proposes to drill through the existing footing and install micropiles using similar methods as illustrated in Alternative 3.
- After the micropiles are installed, drill and grout holes into the existing pier cap and install dowel bars. To alleviate the moment failure from the unreinforced footing seen in Alternative 3, a pier jacket varying in width from 2'-3" at the base of the cap to 2'-11" at the top of the cap will be placed from the top of the footing to the top of the cap.
- The overall width of pier jacket will decrease from 11'-10" at the top of the footing to 8'-10" at the top of the cap.
 - Increasing the pier size will strengthen the pier, extending the design life of the bridge.
 - However, it will significantly increase the weight of the piers, requiring more micropiles, and decrease the hydraulic opening at the proposed column.

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Alternative 4, Micropile with Pier Jacket



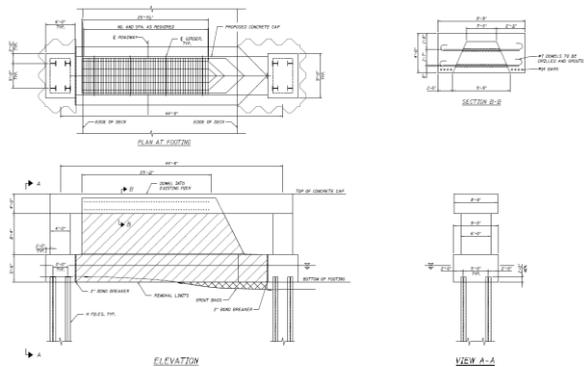
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Alternative 5, Cast-In-Place Pier Cap Retrofit

- Alternative 5 constructs a "new" pier utilizing new footings and pier columns on the outer limits of the existing pier.
- The existing pier cap is retained and incorporated into construction of the new pier cap. The proposed pier footings can be supported by any deep foundation, H-piles, drilled shafts, or micropiles.
- The pier cap will be designed such that the entire load would be carried by the new cap and new reinforcement. Once the new cap is fully cured, the existing pier stem and footing may be removed.
- This solution would create an entirely new load path to a deep foundation and presents structural benefits.
- However, this solution would be difficult to construct and there would be temporary support requirements in order to replace the bearings and properly transfer load to the new cap.

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Alternative 5, Cast-In-Place Pier Cap Retrofit



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Alternative 6, Straddle Bent Pier Retrofit

- Alternative 6 is similar to alternative 5 except that a steel transverse straddle bent is used for the new pier cap in lieu of the cast-in-place options.
- After constructing the proposed columns and footings, Alternative 6 will place two transverse support girders on the proposed columns. These transverse girders will support the bridge during the removal of the existing pier.
- After the existing pier has been removed, longitudinal diaphragms will be installed beneath the four existing girders. Bearings will be installed on the longitudinal girders which will then transfer load to the support girders.
- While this solution also creates an entirely new load path, there are a few challenges. The transverse steel beams could end up as rather large members after all design is complete and these members would also be fracture critical (which creates increased inspection requirements).

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Permits

- Section 4f Permit
 - Required for clearance from:
 - Park
 - Recreation Area
 - Wildlife & Waterfowl Refuge
- There was a Freeman Forest Preserve (FFP) located to the South of the bridge and we needed the bike path in it to access the construction site.
- WHA coordinated with FHWA through IDOT and OWJ (Official with Jurisdiction) to get the permit.

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Permits

- Bridge Condition report (BCR)
 - For funding approval
- Preliminary Bridge Design & Hydraulic Report (PBDHR)
- Army Corp Permit (USACE)
 - For getting into the river
- Office of Water Resources (OWR) & Illinois Environmental Protection Agency (IEPA) Permits
 - For causeway permits
- Project Development Report (PDR)
- WHA initiated all the permits in advance to make sure the contractor does not have to get any permits and there was no delay in construction.

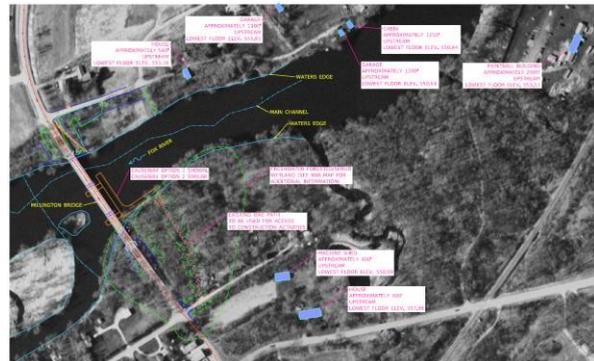
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Hydraulic Analysis

- Hydraulic modeling was performed to determine the effect the proposed causeways, spurs and cofferdams will have on the water surface elevations and subsequently on nearby properties/houses.
- The design criteria for the causeways was based on creating no impact on the base flood event and minimizing created head while still allowing access to construction equipment for a wide range of flows.
- The temporary causeways and cofferdam obstructions were designed to provide approximately one foot of freeboard for the structures above the five-year event.

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Hydraulic Analysis



Hydraulic Impact

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Bike Path



Bike path used to access the construction site.

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Causeway

- Causeway was utilized in the installation of the cofferdams and temporary deck supports, demolition of the existing pier stems and construction of the new pile supported footings and pier stems.
- The project was permitted for two causeway options to give the Contractor a choice on which one would be the easiest and cheapest to construct.
 - Option #1a consists of using an old bike path on the Southeast side of the bridge to gain access to the river and construct a causeway to both piers.
 - Option #1b consists of using the bike path on the Southeast side of the bridge to build a causeway to the South Pier and using a clearing on the Northeast side of the bridge to build a causeway to the North Pier.

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Causeway

WATERWAY DIMENSION TABLE
Causeway The Causeway

(Note: Existing and Proposed conditions do not include causeways, but represent before and after construction conditions.)

Client: C&I (Bridge Dept)
 Project: 17-0112-00-BB
 Contract: 100000
 Prepared by: T&E, Malabar Associates
 Date: 6/22/2017

(Note: The National NRE was taken at the approach face of the bridge. The channel bed was taken at the approach section of the bridge. Flows are for 100-year flood flow. Existing water surface is obtained by HEC-RAS utilizing the slope correction method. All Elevations are based on NAVD83.)

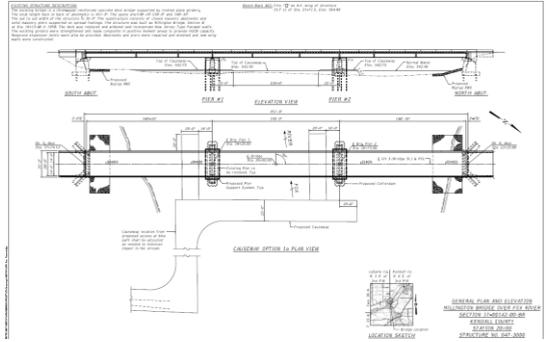
Channel Name	Flow Direction	Elev. (ft)	Existing		Prop.		DEAGULATED SL											
			Bank	Prop.	Bank	Prop.	in Causeway 1	in Causeway 2	in Causeway 3	Edge	Prop.	in Causeway 1	in Causeway 2	in Causeway 3				
Causeway 1 Channel	1	355.0	352.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Causeway 2 Channel	2	355.0	352.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Causeway 3 Channel	3	355.0	352.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Bridge		355.0	352.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Bank		355.0	352.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Water		355.0	352.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Causes of Block Pier Substitution

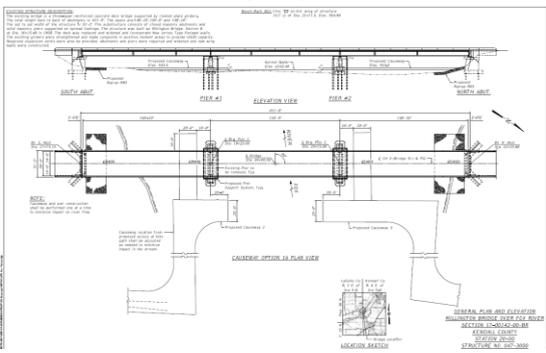
EXISTING STRUCTURE	PROPOSED STRUCTURE
Type: Closed abutments	Type: Closed abutments
Length: 40' back back abutments	Length: 40' back back abutments
Span: 2	Span: 2
Low Head: None	Low Head: None
Scam: None	Scam: None

Waterway Table

Causeway Option 1a



Causeway Option 1b



Causeway



Causeway

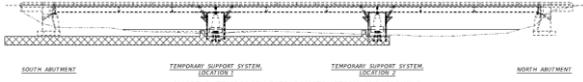


Causeway



Construction of Causeway to the access the bridge

Proposed Construction Sequence



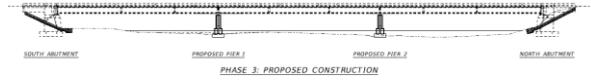
PROPOSED CONSTRUCTION SEQUENCE:

PHASE 2: TEMPORARY PIER CONSTRUCTION AND JACKING

- 5) Erect Steel for Temporary Support System, Location 2
- 6) Jack girders to transfer bridge support to Temporary Support System, Location 2
- 7) Remove designated/remaining portions of Existing Pier 2 (including designated grout bags)
- 8) Drive Proposed Pier 2 Piles
- 9) Drive and install Proposed Pier 2 Cofferdam sheets
- 10) At Pier 1, preform Steps 5-9 for Temporary Support System, Location 1 simultaneously with Location 2

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Proposed Construction Sequence



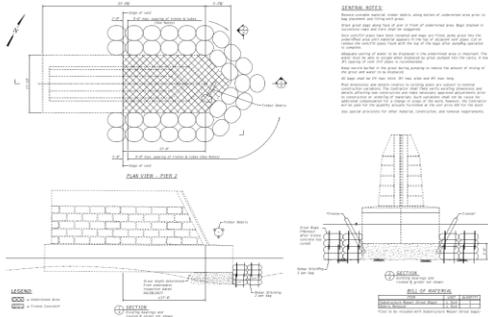
PROPOSED CONSTRUCTION SEQUENCE:

PHASE 3: PROPOSED CONSTRUCTION

- 11) Excavate Cofferdams, pour seal coat concrete, cure, and dewater
- 12) Construct proposed pier footings and cure
- 13) Construct proposed pier walls and cure
- 14) Install retrofit pier bearings
- 15) De-jack/disassemble temporary piers
- 16) Remove all temporary support system items and cutoff temporary pile per the Special Provisions
- 17) Install riprap
- 18) Perform designated deck repairs

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Perform Grout Repair & Remove debris



- Contractor jetted all the mud before performing grout repairs.
- Grout repair was also necessary to install piles and prevent shaking of the existing pier.
- There was a flood during the construction work. Since, the existing pier was stabilized using the grout bags around it, the bridge was still under operation, but the traffic was limited to only normal weight traffic, i.e., less than 5 tons.
- Contractor proposed an alternative method to stabilize the pier utilizing steel plates and we approved it.

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Perform Grout Repair & Remove debris



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Perform Grout Repair & Remove debris



71

Perform Grout Repair & Remove debris



72

Perform Grout Repair & Remove debris



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Perform Grout Repair & Remove debris



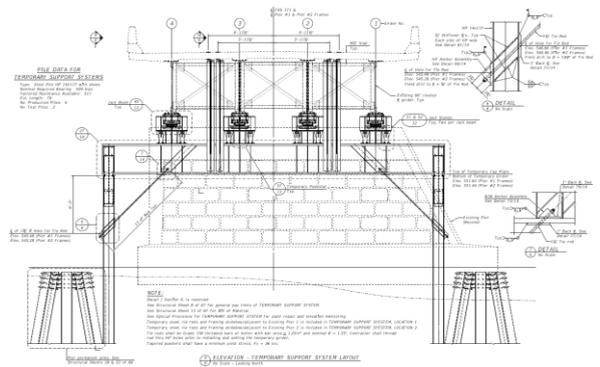
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Perform Grout Repair & Remove debris



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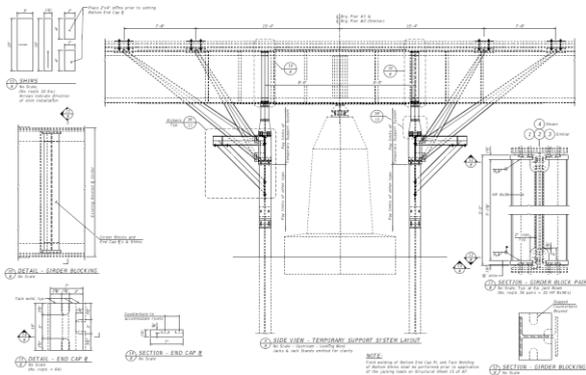
Temporary Support System



The transverse beam was W36x395.

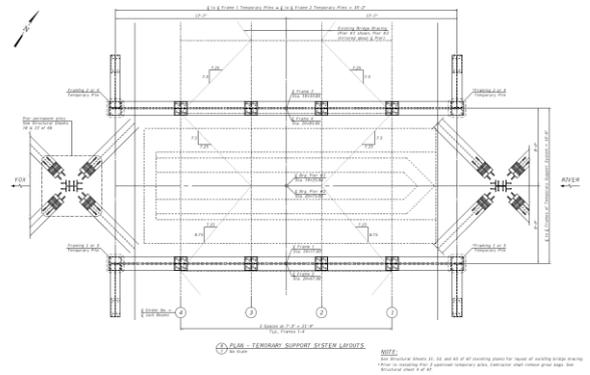
76

Temporary Support System



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Temporary Support System



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Temporary Support System



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Temporary Support System



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Temporary Support System



Use of kickers to provide stability for the beams in the temporary steel support system

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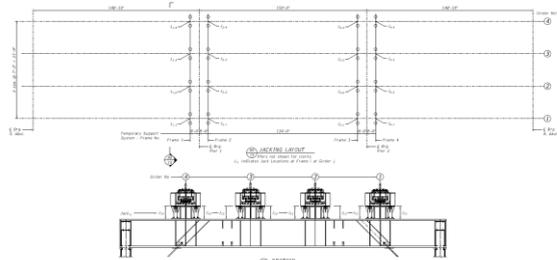
Temporary Support System



Holes for the brace were slotted.

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Jacking

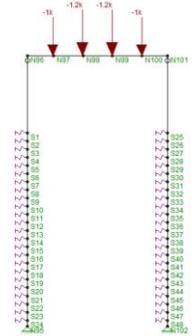


Item	Steel Decking		Reinforcing Steel												Deck Concrete	
	QTY	UNIT	QTY	UNIT	QTY	UNIT	QTY	UNIT	QTY	UNIT	QTY	UNIT	QTY	UNIT	QTY	UNIT
1. Deck Slab Reinforcing Steel	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON
2. Deck Slab Reinforcing Steel	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON
3. Deck Slab Reinforcing Steel	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON
4. Deck Slab Reinforcing Steel	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON
5. Deck Slab Reinforcing Steel	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON
6. Deck Slab Reinforcing Steel	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON
7. Deck Slab Reinforcing Steel	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON
8. Deck Slab Reinforcing Steel	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON
9. Deck Slab Reinforcing Steel	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON
10. Deck Slab Reinforcing Steel	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON	1000.00	TON

Use of hydraulic jack to lift the bridge deck and girder during construction work

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Jacking



When the bridge was lifted upwards using the hydraulic jack, the steel frame would deflect downwards to take the load. Thanks to the iterative solution that we came up with and we were finally able to design the frame to take this effect into account.

Jacking Analysis

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Jacking



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Jacking



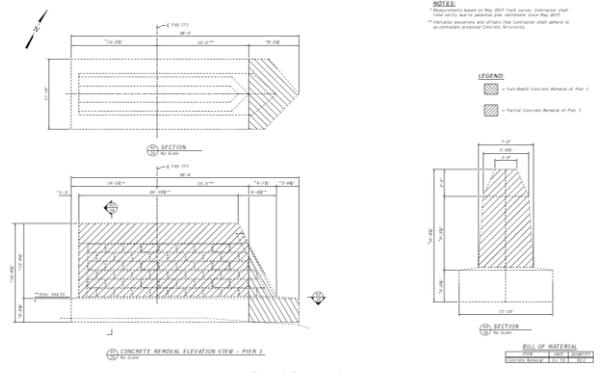
86

Jacking



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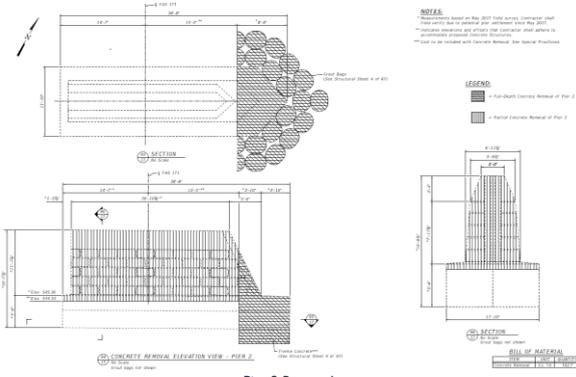
Existing Pier Removal



Pier 1 Removal

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Existing Pier Removal



Pier 2 Removal

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Existing Pier Removal



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Existing Pier Removal



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Existing Pier Removal



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Cofferdam Installation



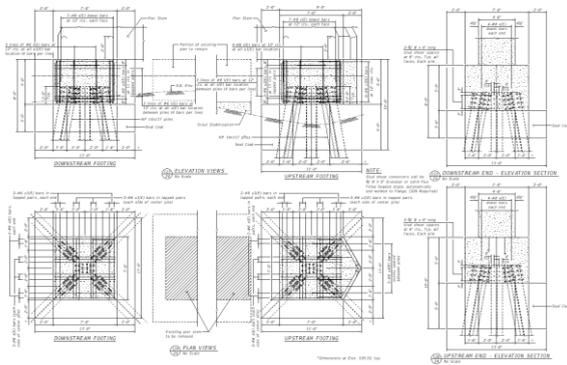
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Cofferdam Installation



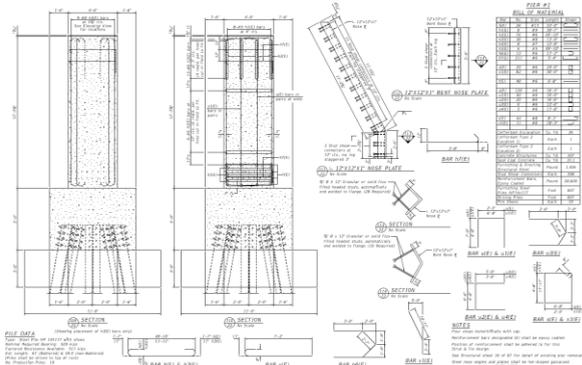
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Driving Proposed Piles



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Driving Proposed Piles



Proposed piles were HP 14X117 and 60' long driven to refusal.

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Construct Proposed Footings



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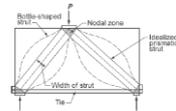
Construct Proposed Footings



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Strut & Tie Pier

- Strut-tie model of piers resting on two battered pile support system.
- Strut-and-tie method was suitable in this case as it can efficiently transfer the load from the superstructure to the footing below.
- Strut-tie model for beam is a concept of designing the deep beams where the load path within the structural member is idealized in the form of truss system.

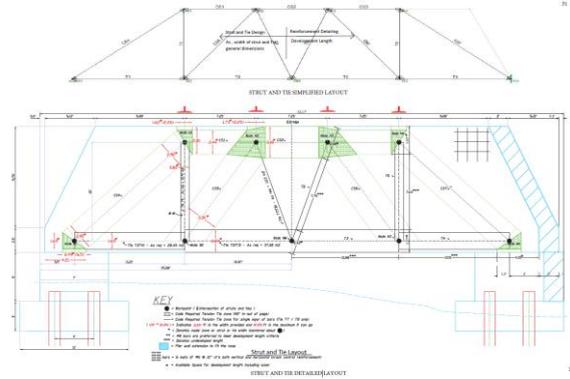


Description of Strut-and-tie model

Source: ACI 318-14

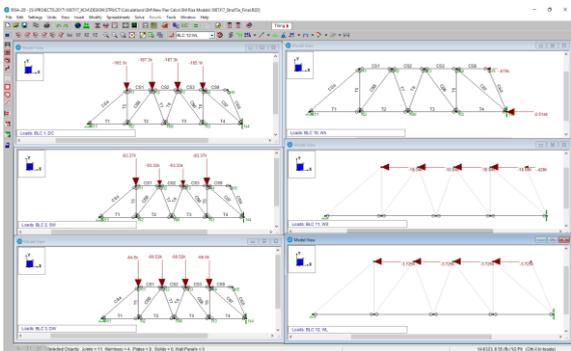
105

Strut & Tie Pier



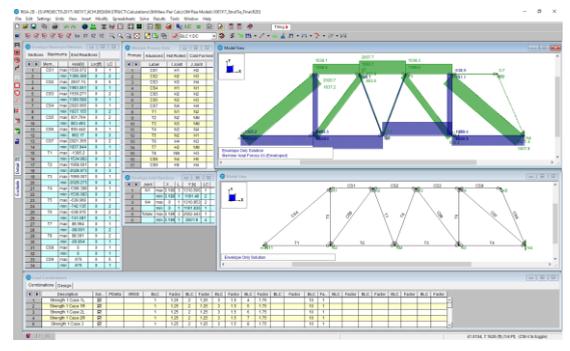
106

Strut & Tie Pier



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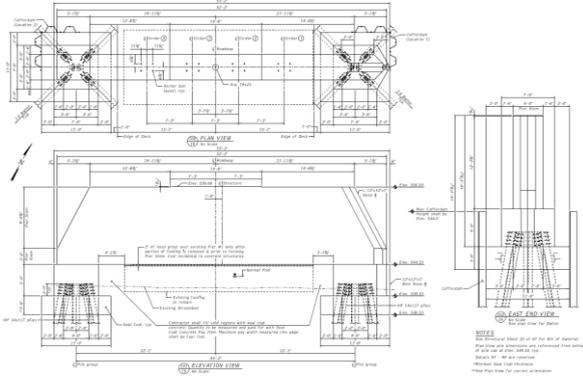
Strut & Tie Pier



RISA Model

108

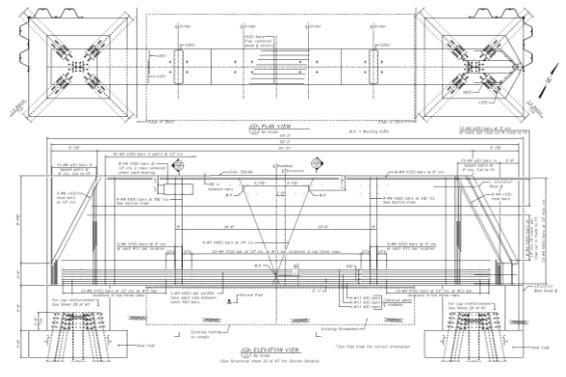
Struct & Tie Pier



Existing footing was assumed to provide no bearing.

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Struct & Tie Pier



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Struct & Tie Pier



Removal of existing pier

111

Struct & Tie Pier



Existing footing used as a base to construct proposed pier.

112

Struct & Tie Pier



Reinforcement Mat

113

Struct & Tie Pier



Reinforcement Mat

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Struct & Tie Pier



Reinforcement Mat

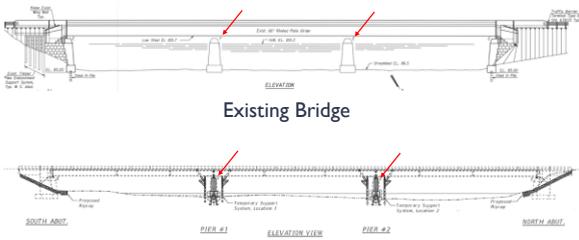
115

Struct & Tie Pier



116

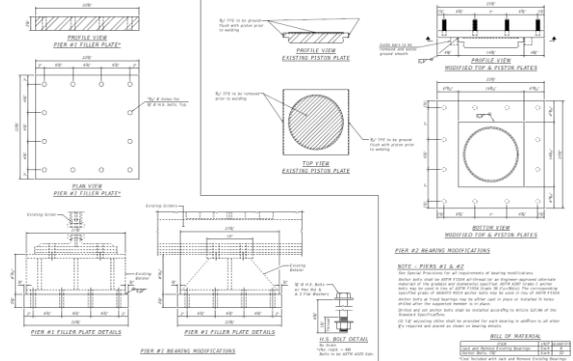
Bearing Modifications



Both the piers resist equal force.

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Bearing Modifications



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Bearing Modifications



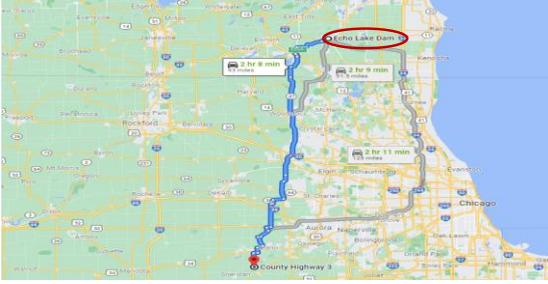
119

Disassemble Temporary Support System



120

Constructability Challenges



There is a dam upstream of the bridge and the Army Corps would release water during heavy rains. This would raise water level unexpectedly and flood the causeway.

121

Constructability Challenges



We were not able to do any construction work because of the flooding for 1 construction season.

122

Conclusion

- Despite many challenges, we were able to replace the Millington Bridge Piers and it is under operation carrying the loads efficiently.
- We were able to incorporate the concept of strut-and-tie model of beam in this new pier design and construction with battered piles foundation at the ends.

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Conclusion



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Millington Bridge Pier Replacement

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Questions?



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